

Dynegy Midwest Generation, LLC 1500 Eastport Plaza Drive Collinsville, IL 62234

February 8, 2024

Illinois Environmental Protection Agency DWPC – Permits MC#15 Attn: Part 845 Coal Combustion Residual Rule Submittal 1021 North Grand Avenue East Springfield, IL 62794

Re: Baldwin Power Plant Fly Ash Pond System; IEPA ID # W1578510001-01-02-03

Dear Mr. LeCrone:

In accordance with Title 35 of the Illinois Administrative Code (35 I.A.C.) Section (§) 845.650(e), Dynegy Midwest Generation, LLC is submitting this alternative source demonstration (ASD) for exceedances observed from the Quarter 3 2023 sampling event at the Baldwin Power Plant Fly Ash Pond System, identified by Illinois Environmental Protection Agency (IEPA) ID No. W1578510001-01, -02, and -03. This ASD is being submitted within 60 days from the date of determination of an exceedance of a groundwater protection standard (GWPS) for constituents listed in 35 I.A.C. § 845.600. As required by 35 I.A.C. § 845.650(e)(1), the ASD was placed on the facility's website within 24 hours of submittal to the agency.

The ASD determined that groundwater quality at compliance well MW-253 was compromised due to faulty well construction. Review of the data included in the ASD identified two additional wells within the existing monitoring system that appear to be compromised due to faulty well construction - background location MW-306 and compliance well MW-350. The following actions are proposed to resolve this issue:

- Compliance wells MW-253 and MW-350 will be abandoned and replaced with new monitoring wells located within 10 feet of the original well locations with similar well construction (the well screens will monitor the same hydrostratigraphic unit)
- Background well MW-306 will be abandoned and will not be replaced. There are two other background monitoring wells (MW-304 and MW-358) which provide sufficient background monitoring data that meet the requirements of 35 I.A.C. § 845.630(a)(1)
- 3. In recognition of the compromised data collected from background well MW-306, results collected from this well will be removed from the background dataset that applies to both the Baldwin Bottom Ash Pond and the Fly Ash Pond System. Background statistics will be recalculated using the two remaining background wells (MW-304 and MW-358) for use in determination of exceedances starting with data collected in the first quarter of 2024 until a revised groundwater monitoring plan is submitted for approval.
- 4. Following abandonment and well replacement activities, a revised groundwater monitoring plan will be submitted no later than the second quarter of 2024 which will include updated background statistics using only data from retained background wells MW-304 and MW-358.

Later this month Dynegy Midwest Generation, LLC will be providing a follow-up submittal further detailing the proposed actions to resolve this issue.

One hard copy of the ASD is provided with this submittal.

Sincerely,

Phil Morris, PE Senior Director, Environmental

Enclosures

Alternative Source Demonstration, Baldwin Power Plant Fly Ash Pond System, Baldwin Power Plant, Baldwin, Illinois. February 2024



engineers | scientists | innovators

ALTERNATIVE SOURCE DEMONSTRATION

Baldwin Power Plant Fly Ash Pond System (Unit ID #605) IEPA ID: W1578510001-01, -02, -03 35 IAC 845.650

Prepared for

Dynegy Midwest Generation, LLC 1500 Eastport Plaza Drive Collinsville, Ilinois 62234

Prepared by

Geosyntec Consultants, Inc. 500 W Wilson Bridge Road, Suite 250 Worthington, OH 43085

Project Number: GLP8068

February 6, 2024



Alternative Source Demonstration

Baldwin Power Plant Fly Ash Pond System (Unit ID #605) IEPA ID: W1578510001-01, -02, -03 35 IAC 845.650

Prepared for

Dynegy Midwest Generation, LLC 1500 Eastport Plaza Drive Collinsville, Illinois 62234

Prepared by

Geosyntec Consultants, Inc. 500 W. Wilson Bridge Road Worthington, OH 43085

License No.: 062.040562 Expires: 11/30/2025

John Seymour, P.E.

John Seymour, P.E Senior Principal

Project Number: GLP8068

February 6, 2024





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ACRONYMS AND ABBREVIATIONS

ASD	alternative source demonstration
BAP	Bottom Ash Pond
bgs	below ground surface
BPP	Baldwin Power Plant
CCR	coal combustion residuals
cm/s	centimeters per second
DMG	Dynegy Midwest Generation, LLC
EPRI	Electric Power Research Institute
FAPS	Fly Ash Pond System
GWPS	groundwater protection standard
IAC	Illinois Administrative Code
IEPA	Illinois Environmental Protection Agency
LOE	line of evidence
mg/L	milligrams per liter
NAVD88	North American Vertical Datum of 1988
NPDES	National Pollutant Discharge Elimination System
NRT	Natural Resource Technology, Inc.
SU	standard units
USEPA	United States Environmental Protection Agency

February 2024



1. INTRODUCTION

Geosyntec Consultants, Inc. has prepared this alternative source demonstration (ASD) on behalf of Dynegy Midwest Generation, LLC (DMG), regarding the Fly Ash Pond System coal combustion residuals (CCR) unit at the Baldwin Power Plant (BPP) near Baldwin, Illinois. The ASD is completed pursuant to the Illinois Administrative Code (I.A.C.) Title 35, § 845 ("Standards for the Disposal of CCR in Surface Impoundments") and was completed by February 8, 2024 within 60 days of determination of the exceedances (December 10, 2023), as required by 35 I.A.C. § 845.650(e). This report applies specifically to the CCR Unit referred to as the Fly Ash Pond System (FAPS), identification (ID) number (No.) 605, Illinois Environmental Protection Agency (IEPA) ID No. W1578510001-01, -02, -03, and National Inventory of Dams (NID) ID No. IL50721. This ASD was prepared in conformance with guidance provided in the Electric Power Research Institute (EPRI) guidance for development of ASDs at CCR sites (EPRI 2017), guidance provided by the United States Environmental Protection Agency (USEPA, 2015; USEPA 2016), and others (Miller 2019).

A pH exceedance of 11.3 standard units (SU) was identified above the site-specific groundwater protection standard (GWPS) of 11.1 SU at monitoring well MW-253 following the Third Quarter (Q3) 2023 sampling event (Ramboll 2023a). No exceedance of pH was identified for the Second Quarter at monitoring well MW-253 because no groundwater sample could be collected due to problems with the dedicated bladder pump.

Under 35 I.A.C. 845.650(e), the owner or operator of a CCR surface impoundment may submit a demonstration that a source other than the CCR surface impoundment caused the contamination and the CCR surface impoundment did not contribute to the contamination, or that the exceedance of the groundwater protection standard resulted from error in sampling, analysis, or statistical evaluation, natural variation in groundwater quality, or a change in the potentiometric surface and groundwater flow direction.

Pursuant to 35 I.A.C. 845.650(e), the lines of evidence (LOEs) documented in this ASD demonstrate that a source other than the BPP FAPS CCR unit was the cause of the GWPS exceedance for pH at monitoring well MW-253. Grout infiltration potentially from well installation, low magnesium/calcium ratios indicative of grout infiltration, and low concentrations of CCR indicator parameters are three lines of evidence (LOEs) which indicate that the pH exceedance at MW-253 appears to be due to sampling error (due to improper well construction) and not a release from the Baldwin FAPS.

2. BACKGROUND

2.1 Site Location and Description

The BPP is located in Randolph County and St. Clair County in southwest Illinois approximately 0.5 miles west-northwest of the village of Baldwin. The BPP property is bordered by Baldwin Road to the east; the village of Baldwin to the southeast; Illinois Central Gulf railroad tracks, State Road 154, and scattered residences to the south; the Kaskaskia River to the west; and farmland to the north. CCR impoundments present at the BPP include the Bottom Ash Pond (BAP) and the closed FAPS.

Non-CCR impoundments present at the BPP include the Secondary Pond, Tertiary Pond, and Baldwin Lake (BPP Cooling Pond). The location of the CCR and non-CCR impoundments are shown in **Attachment 1**. The FAPS is a closed in-place CCR unit approved for closure by the IEPA on August 16, 2016. Closure was completed on November 17, 2020 (DMG 2020). Prior to closure, the FAPS was comprised of the West Fly Ash Pond, East Fly Ash Pond, and Old East Fly Ash Pond.

2.2 Description of the CCR Unit

The BPP began operation in 1970 and initially burned bituminous coal from Illinois, switching to subbituminous coal in 1999. The FAPS is an unlined surface impoundment, with a surface area of approximately 263 acres. The external perimeter of the three subunits within the FAPS was originally constructed in 1969. The Old East Fly Ash Pond and East Fly Ash Pond were used to store and dispose of fly ash from the BPP, while the West Fly Ash Pond was used to store and dispose of dry-stacked fly ash and to clarify CCR contact stormwater (AECOM 2016).

2.3 Geology and Hydrogeology

Significant site investigation has been completed to fully characterize the geology, hydrogeology, and groundwater quality as provided in the Supplemental Hydrogeologic Site Characterization and Groundwater Monitoring Plan (Natural Resource Technology, Inc. [NRT] 2016), the Hydrogeologic Site Characterization Report (Ramboll 2021), and the Hydrogeologic Site Characterization 1 (Ramboll 2023b). These materials are incorporated herein.

Three hydrostratigraphic units are present at the BPP, which include the CCR, an unconsolidated Upper Unit, and a Bedrock Unit.

- CCR: Consists primarily of bottom ash, fly ash, and boiler slag and also includes fill materials comprising predominantly of clays and silts excavated on-site for use in berm and road construction around the impoundment.
- Upper Unit: Predominantly clay with silt and minor sand, silt layers, and occasional sand lenses, and includes lithologies identified as the Cahokia Formation, Peoria Loess, Equality Formation, and Vandalia Till. Thin sand seams present at the contact between the Upper Unit and Bedrock Unit have been identified as potential migration pathways

(PMPs) due to higher hydraulic conductivities in comparison to those in the surrounding clays (e.g., 10⁻⁴ centimeters per second [cm/s] in sands compared with 10⁻⁵ cm/s in clays) (Ramboll 2023a). Continuous sand seams have not been observed in the Upper Unit or immediately adjacent to the FAPS. Due to the predominance of clay and only thin and intermittent sand lenses, this unit is not considered a continuous aquifer unit within the site boundary.

• Bedrock Unit: Pennsylvanian and Mississippian-aged interbedded shale and limestone continuously underlies the BPP and is considered the uppermost aquifer at the site. The top of bedrock ranges from 12.5 feet below ground surface (bgs) near the Kaskaskia River to 70 feet bgs underlying the East Fly Ash Pond (part of the FAPS). The Bedrock Unit is the uppermost aquifer.

Groundwater at the site has previously been classified as Class II groundwater in accordance with 35 IAC 620 based on the geometric mean hydraulic conductivity values measured in the monitoring wells screened in both the Upper Unit $(3.2 \times 10^{-5} \text{ cm/s})$ and the Bedrock Unit (5.0×10^{-6}) (NRT 2014).

The groundwater monitoring network for the FAPS consists of 18 monitoring wells: 15 downgradient compliance monitoring wells (MW-150, MW-151, MW-152, MW-153, MW-252, MW-253, MW-350, MW-352, MW-366, MW-375, MW-377, MW-383, MW-384, MW-390, and MW-391) and three background monitoring wells (MW-304, MW-306, and MW-358) (**Attachment 1**). Monitoring wells are screened in both the unconsolidated unit from elevation 369 to 432 feet North American Vertical Datum of 1988 (NAVD88) (MW-150, MW-151, MW-152, MW-153, MW-252, and MW-253) and the uppermost aquifer (Bedrock Unit; all other monitoring network wells) from approximately elevation 348 to 408 feet NAVD88.

Groundwater flow in the UA is west to northwest in the east area of the FAPS until groundwater reaches the bedrock valley feature underlying the Secondary and Tertiary Ponds west of the FAPS, at which point the flow direction veers southwest towards this bedrock surface low (Attachment 2). Groundwater flow directions are generally consistent across seasons.

3. ALTERNATIVE SOURCE DEMONSTRATION LINES OF EVIDENCE

This ASD for the pH GWPS exceedance at MW-253 is based on three LOEs. These LOEs are described and supported below.

3.1 LOE #1: Grout Infiltration Due to a Poor Seal During Installation Can Result in Elevated Groundwater pH.

The recorded pH values at MW-253 have varied between 9.8 SU and 12.4 SU since 2015. These values are consistently elevated compared to the other monitoring wells in the immediate vicinity of MW-253 (i.e., MW-152, MW-153, MW-304, MW-352, MW-377, and MW-384) (Figure 1; Attachment 1). This includes monitoring well MW-153, which is co-located with MW-253 but screened at a shallower interval (Attachment 3). If the FAPS were the source of the elevated pH, it would be expected to influence shallower wells nearer to the unit as well as impacting MW-253. Therefore, the pH values at MW-253 are anomalously elevated and appear to be an isolated issue associated with improper well construction.

Bentonite grout slurry, which often contains large proportions of calcium hydroxide (Ca(OH)₂) due to the inclusion of cement, was used during well construction to generate a seal above the filter pack at MW-253 (**Attachment 3**). Causes of grout contamination can include fracturing of the grout seal during curing, shrinking of the grout seal away from the casing, or bridging of the grout during placement. If the grout seal is not successfully placed during well installation, it can result in migration of the grout into the filter pack of the screen or surrounding aquifer. Bentonite grout contamination generally increases the pH of groundwater as it migrates across the filter pack and into the well (Aller et. al 1991, FDEP 2005); this is attributed to the dissolution of hydroxide ions from the cement (Blackmer 1988).

Anomalously elevated pH levels at MW-253 (**Figure 1**) appear to be an isolated issue, indicating that the well may have experienced construction issues permitting the infiltration of grout into the proximal groundwater and is not truly representative of naturally occurring distal groundwater unaffected by the well construction. This is supported by the pH behavior at monitoring well MW-352, which was installed by the same drillers during the same event as MW-253 (**Attachment 3**). The recorded pH values at MW-352 (**Figure 1**) were greater than 10.0 SU for the first six events following installation in September 2010 but then underwent a subsequent decline such that they are now consistent with other wells in the vicinity. This pattern suggests that the initial samples at MW-352 may have been affected by grout contamination during well installation which was flushed out during subsequent events. Similar flushing has not been observed at MW-253, likely due to a greater infiltration of grout through the seal and filter pack. The pH trends at MW-253 and MW-352 indicate that the recent pH levels at MW-253 are due to a source other than the FAPS.

3.2 LOE #2: The Low Magnesium/Calcium (Mg/Ca) Ratio at MW-253 is Indicative of Grout Contamination.

When considering the potential for grout contamination of monitoring wells, elevated pH is often correlated with an increase of the proportion of cations associated with the grouting process, particularly calcium (Price 1990). It is anticipated that wells that are affected by grout contamination resulting in a pH of 10 or above would have a notably lower magnesium-to-calcium (Mg/Ca) ratio than those with pH levels less than 10 due to the increasing relative abundance of calcium in groundwater released from the grout (Blackmer 1988).

The Mg/Ca ratio for Q3 2023 at MW-253 was 0.03, which is consistent with wells in other studies where grout contamination was identified as a source of elevated pH in groundwater (Blackmer 1988). The Mg/Ca ratio at MW-253 is notably lower than the surrounding monitoring wells with lower pH values (Mg/Ca ratios ranging between 0.28 to 0.78) (**Figure 2**).¹ The anomalously low Mg/Ca ratio at MW-253 provides further support that grout contamination is the source of high pH values at that location.

3.3 LOE #3: The Low Concentrations of Indicator Parameters at MW-253 Do Not Suggest Influence from the FAPS.

Boron and sulfate are typically considered geochemically conservative parameters due to their limited attenuation by chemical processes in groundwater flow. They therefore function as indicators for potential CCR unit releases due to their high relative concentration in CCR and CCR porewater. Porewater adequately represents the mobile fractions of boron and sulfate from fly ash better than leaching from CCR materials due to variability in leach testing recoveries (Izquierdo and Querol 2012,Wang et al, 2023).

Boron concentrations at MW-253 have been reported at values ranging between 0.03 and 0.24 milligrams per liter (mg/L) for groundwater sampling events completed between November 2010 and July 2023 (**Figure 3**) with concentrations below 0.1 mg/L since 2011. However, boron concentrations collected from temporary CCR porewater piezometers (Attachment 4) representative of the FAPS (TPZ-163, TPZ-167, and TPZ-168) ranged from 36.3 and 94.7 mg/L (NRT 2016), providing evidence that concentrations of boron within the FAPS are over two orders of magnitude higher than the concentrations observed at MW-253. If groundwater at MW-253 had been impacted by CCR from the unit, boron concentrations would be expected to be elevated above the background Upper Tolerance Limit (UTL) of 2.16 mg/L (Ramboll 2023a). Boron

¹ Background well MW-306 and downgradient bedrock well MW-350 also exhibited anomalously high pH and low Mg/Ca values. As these locations are geographically separate from MW-253 and an exceedance for MW-350 was not identified during the Q3 2023 sampling event, the potential for grout contamination at these locations will not be discussed in this report.

concentrations at MW-253 are consistently less than the background UTL (**Figure 3**), indicating that this well has not been affected by CCR.

Similarly, sulfate concentrations at MW-253 were reported at values between 94 and 806 mg/L during sampling events which occurred between November 2010 and July 2023, with concentrations below 200 mg/L since 2019 (**Figure 4**). The sulfate concentrations in the FAPS piezometers (NRT 2016) ranged between 495 mg/L (TPZ-163) and 2,820 mg/L (TPZ-168), which are either comparable to or substantially higher than sulfate concentrations at MW-253, particularly for recent events. If groundwater at MW-253 had been impacted by CCR from the unit, sulfate concentrations would be expected to be elevated above the background UTL of 762 mg/L (Ramboll 2023a). Sulfate concentrations at MW-253 are consistently less than the background UTL (**Figure 4**), indicating that this well has not been affected by CCR.

If the FAPS, which contains concentrations of boron and sulfate over an order of magnitude higher than MW-253, were impacting groundwater quality at MW-253, an increase in boron and sulfate concentrations would be expected. The current boron and sulfate concentrations at MW-253 do not display increasing trends (**Figure 3** and **Figure 4**, respectively) and have concentrations below their respective background UTLS, which suggests that the elevated pH in groundwater at MW-253 is not attributable to the FAPS.



4. CONCLUSIONS

It has been demonstrated that the pH GWPS exceedance at MW-253 is not caused by a release from the FAPS CCR unit and that the unit has not caused or contributed to the exceedance, but instead is attributed to a source other than the FAPS. The alternative source of the pH exceedance at MW-253 is the contamination of the groundwater by the grout used during well construction. The following summarizes the three LOEs used to support this demonstration:

- 1. High pH is expected where grout contamination has occurred from a seal that is not effectively placed.
- 2. A low Mg/Ca ratio can be used as an indicator of grout contamination, and it has been identified at MW-253 where it is lower than the ratio at surrounding monitoring wells. This is caused by the dissolution of grout.
- 3. Low concentrations of FAPS indicator parameters boron and sulfate relative to CCR porewater were detected at MW-253.

This demonstration fulfills the requirement of both 35 IAC 845.650(e) and the technical manual for the Municipal Solid Waste Landfill federal regulatory program (Code of Federal Regulations, Title 40, Section 258) that a statistically significant increase may result from sampling error.

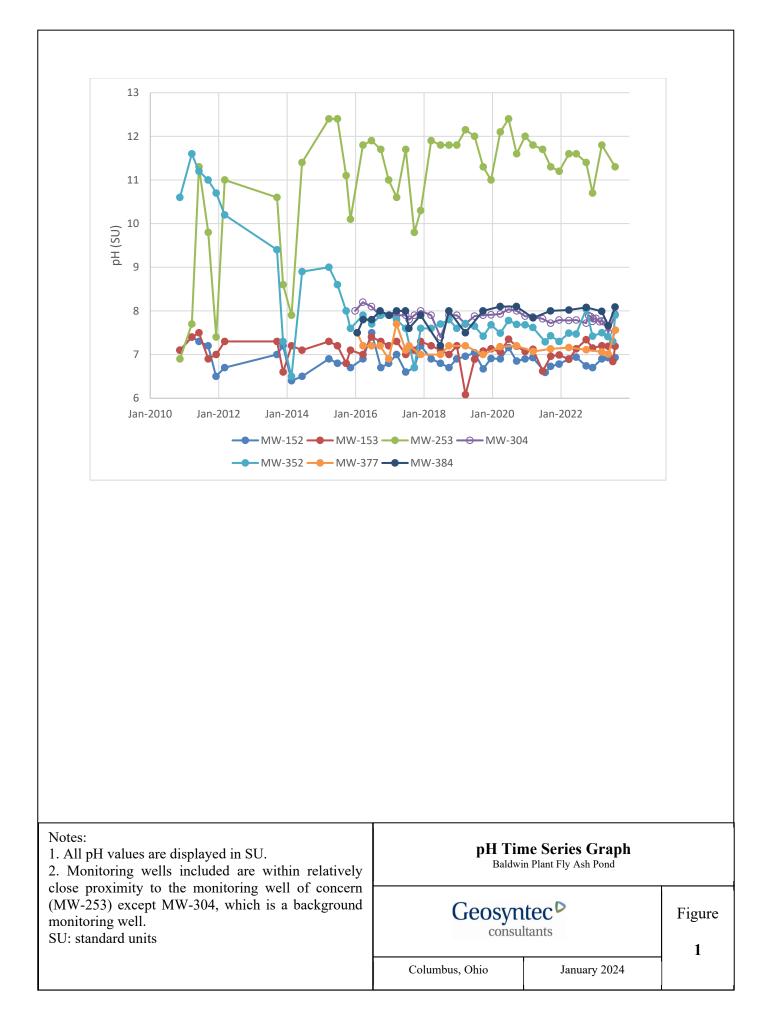
The information serves as the written ASD prepared in accordance with 35 IAC 845.650(e) demonstrating that the GWPS exceedance for pH at MW-253 is not due to the FAPS CCR unit. Therefore, implementation of corrective measures is not required for pH at the FAPS CCR unit.

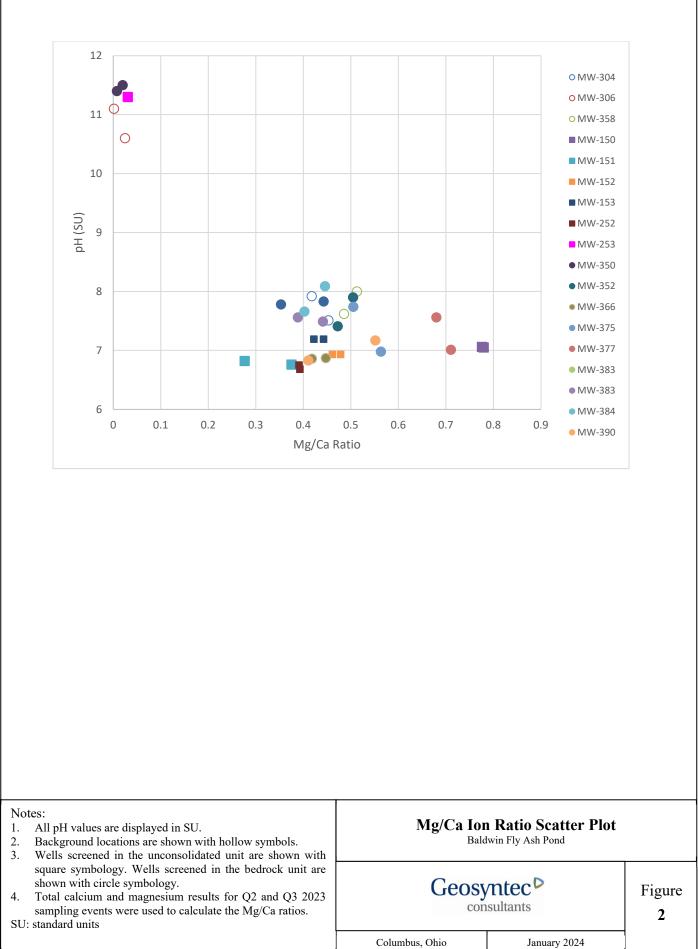
5. REFERENCES

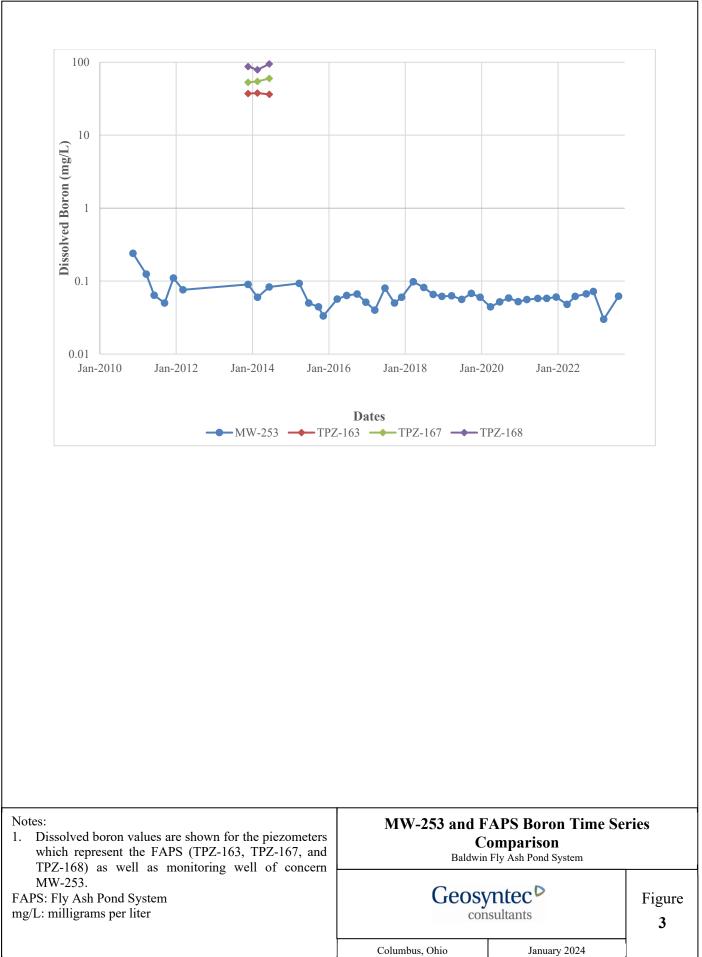
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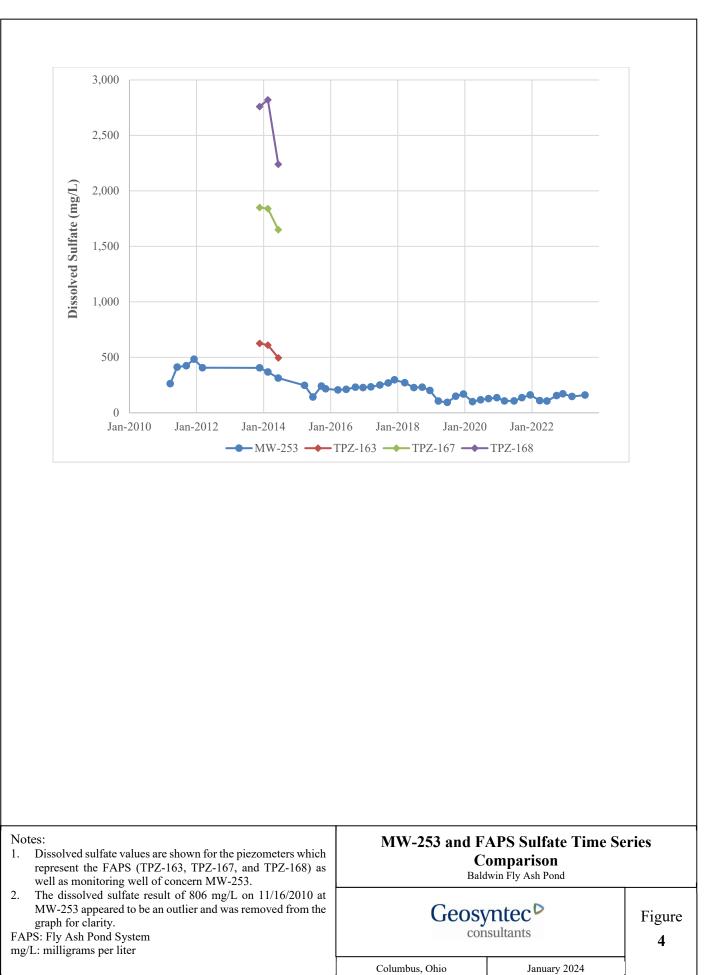
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FIGURES



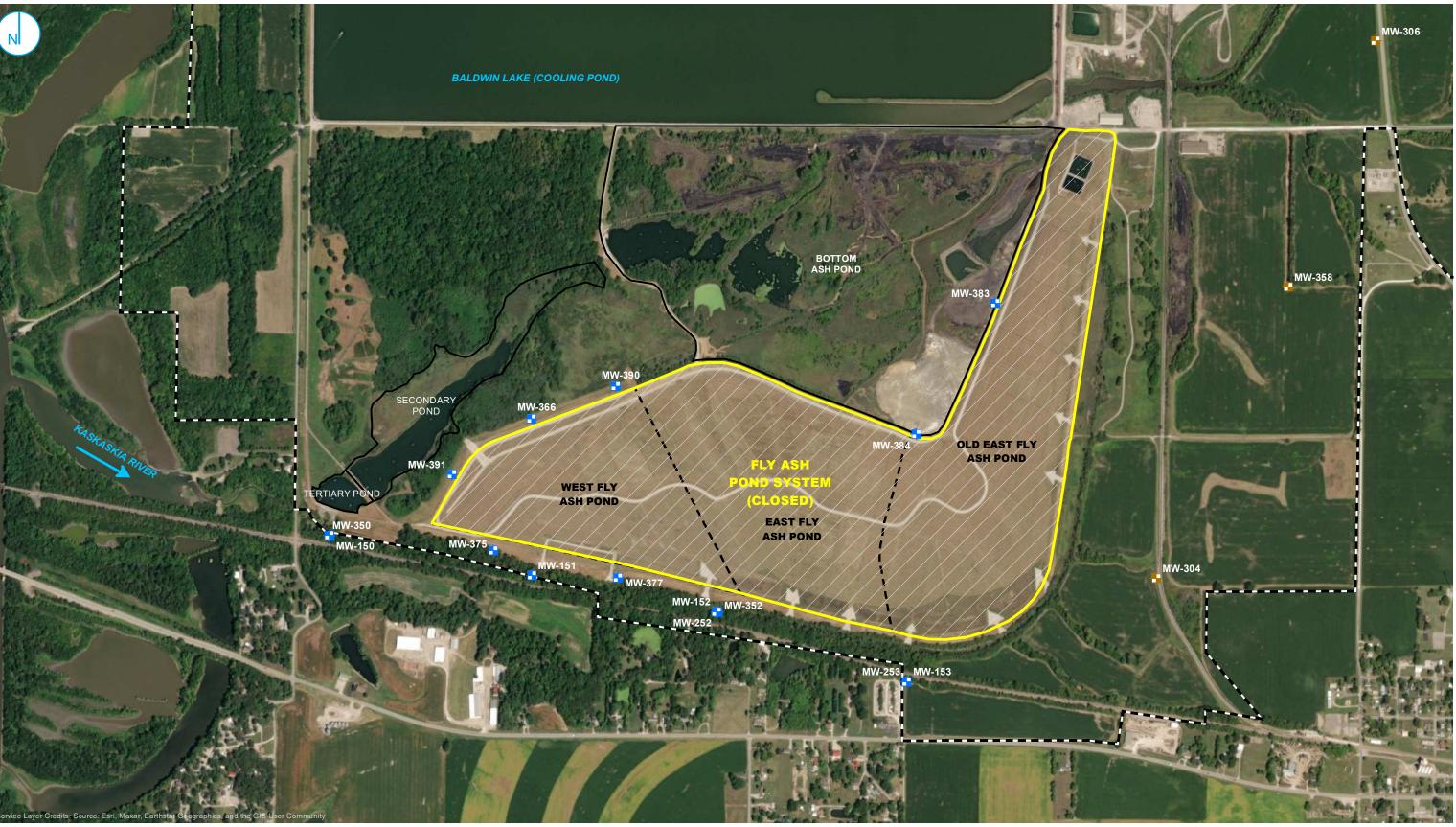






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ATTACHMENT 1 Part 845 Groundwater Monitoring Network



REGULATED UNIT (SUBJECT UNIT) SITE FEATURE CAPPED AREA PROPERTY BOUNDARY

35 I.A.C. § 845 GROUNDWATER

FIGURE 1

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

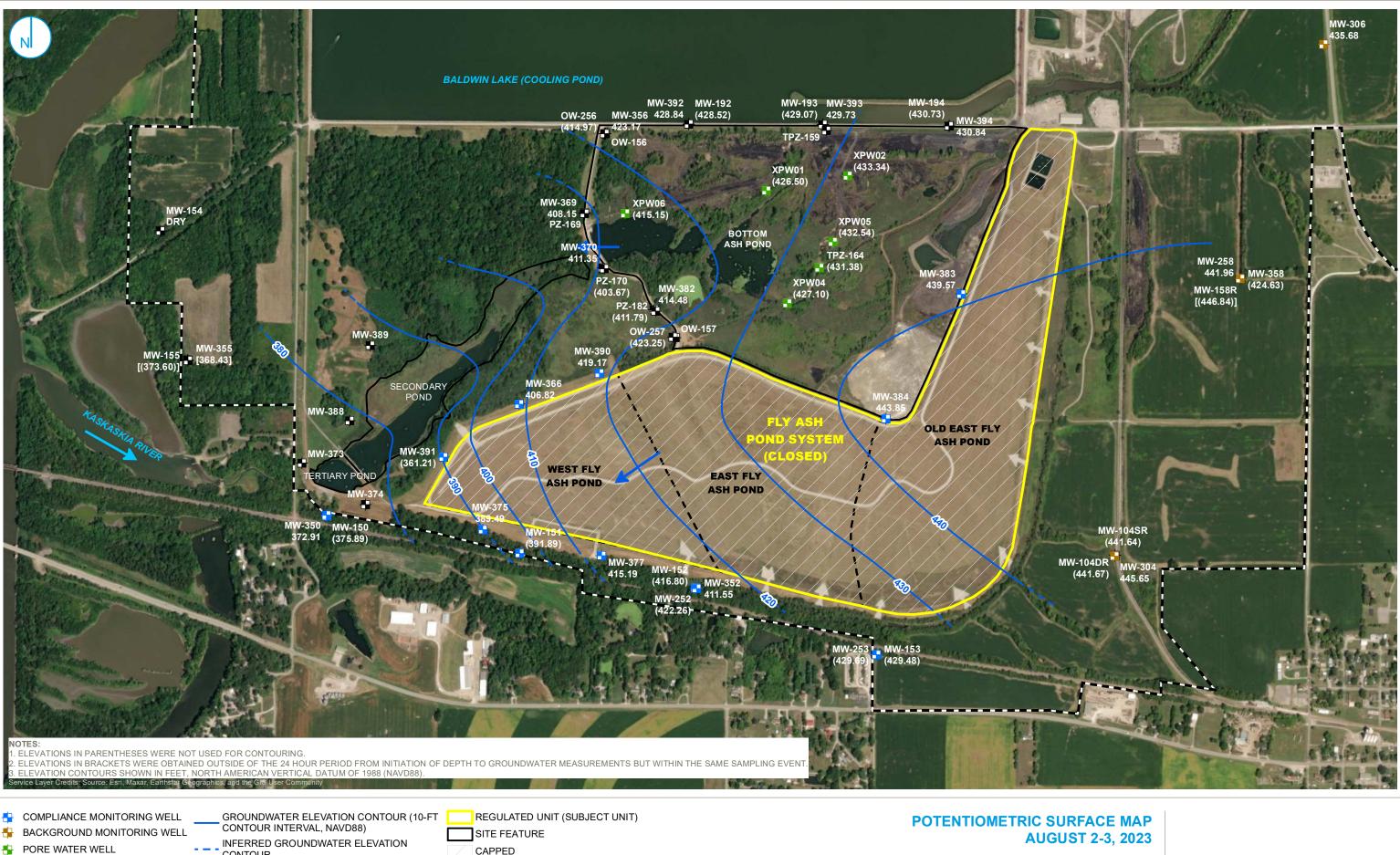


MONITORING WELL NETWORK

FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS

ATTACHMENT 2

Potentiometric Surface Maps – August 2-3, 2023



CONTOUR

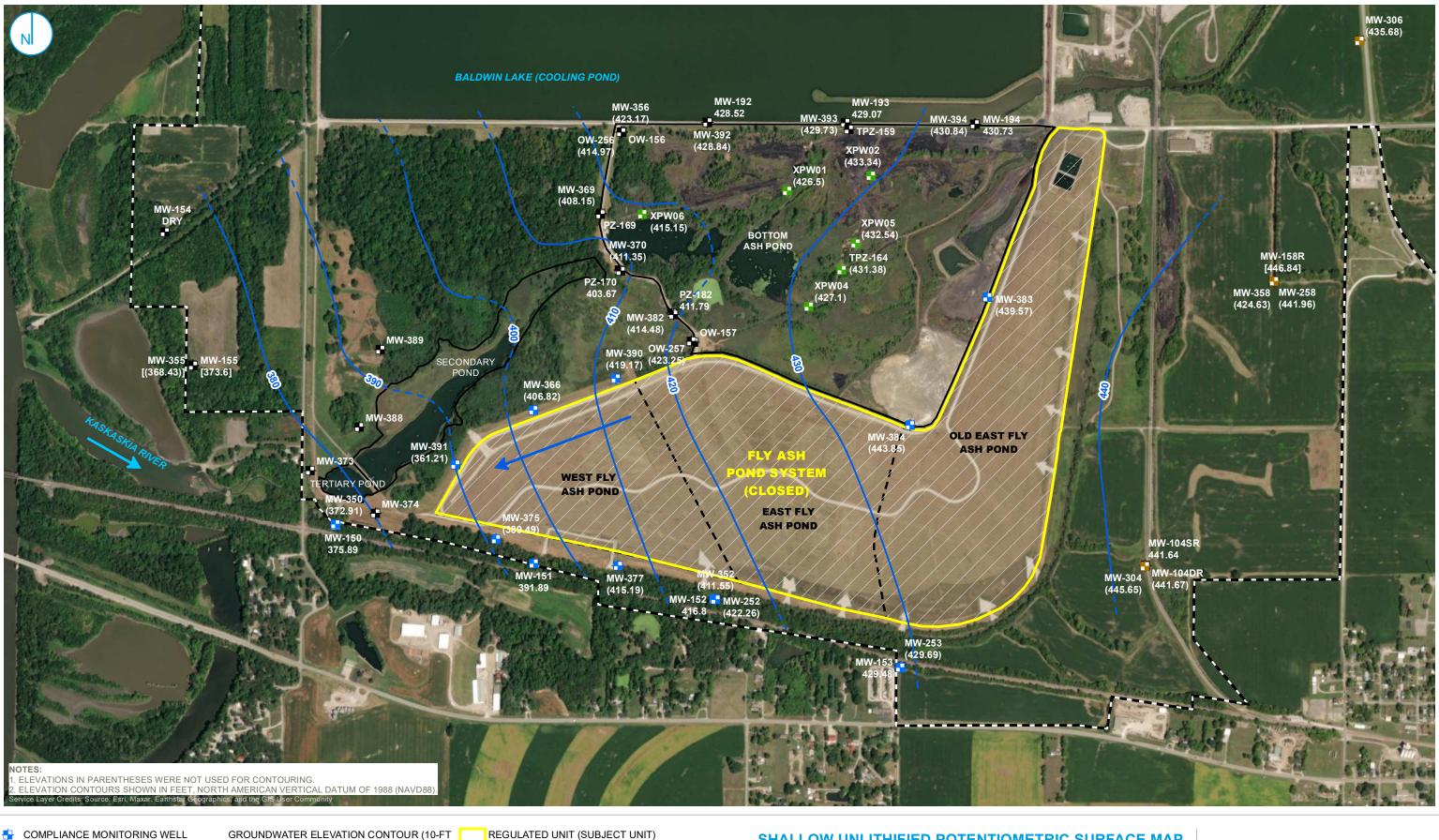
PROPERTY BOUNDARY

2023 ANNUAL GROUNDWATER MONITORING AND CORRECTIVE ACTION REPORT

800 | Foot

FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.





BACKGROUND MONITORING WELL

800

| Foot

- HONITORING WELL
- PORE WATER WELL

400

- CONTOUR INTERVAL, NAVD88) INFERRED GROUNDWATER ELEVATION CONTOUR
- REGULATED UNIT (SUBJECT UNIT) SITE FEATURE
- CAPPED
- PROPERTY BOUNDARY

SHALLOW UNLITHIFIED POTENTIOMETRIC SURFACE MAP AUGUST 2-3, 2023

2023 ANNUAL GROUNDWATER MONITORING AND CORRECTIVE ACTION REPORT **FLY ASH POND SYSTEM** BALDWIN POWER PLANT BALDWIN, ILLINOIS

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



ATTACHMENT 3 MW-153, MW-253, and MW-352 Boring Logs and Well Construction Logs

	KELRON ENVIRONMENTAL		LOG OF BORING MW-153									
	INCORPORATED								(Page 1 of 1)			
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. n: Twp 04S, Rng 07W, 15 SW, SW, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company		'OD / 4 w-Stem	4 1/4" ID /Rotary 60'')		Ge 550) La To		ace Elevation: 442.77 sing Elevation 445.67			
Depth in Feet	DESCRIPTION		Surf. Elev. 442.77	Samples	Recovery inches	Qp TSF	nscs	GRAPHIC	Well: MW-153 Elev.: 445.67			
0 -	Continuous boring - no soil sampling co Refer to boring log for adjacent nested v for a description of subsurface materials	well MW-253	- 442						Concrete			
5 - - -			- 437						Seal Bentonite Chips Riser (Sch 40 PVC)			
- 10 - - -			- 432									
- 15 - - -			- 427						Filter Pack			
- 20 - - -	END BOREHOLE AT 20.5 FEET BLS		- 422						Bottom Cap			
- 25 -												

	KELRON ENVIRONMENTAL INCORPORATED		L	.OG	OF	BOR	ING M	W-253 (Page 1 of 2)			
Ash Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. Location: Twp 04S, Rng 07W, 15 SW, SW, NE		Date Completed : 09/20/2010 Hole Diameter : 8 1/2"OD / 4 1/4" ID Drilling Method : Hollow-Stem/Rotary (CME-550) Sampling Method : MacroCore (60") Drilling Company : PSC					0) Land Sur Top of Ca	Driller : Matt Cooper Geologist : Brendon Wilder (PSC)			
Depth in Feet	DESCRIPTION		Surf. Elev. 442.70	Samples	Recovery inches	Qp TSF	USCS GRAPHIC	Well: MW-253 Elev.: 445.84			
- 0	SILTY CLAY, trace gravel, hard, light br	own, dry	- 442	1	25/48	4.5+					
	- - - hard, medium plasticity, gray (2.5Y 6/1) with 5 - yellow-brown mottling (10YR 5/6), moist			2		4.5+					
-			- 437	3	47/60	4.5	CL				
- 10 -				5	53/60	4.5		Riser (Sch 40 PVC)			
-	CLAY (fat) with SAND, trace gravel, dar with light gray mottling, mottling decreas - grain size analysis @ 11 - 12 ft: 0.7% gravel, 16.4% sand, 41.4% s	ses with depth	- 432	7	33/00	4.0		Grout Bentonite Slurry			
				9	52/60	3.0	сн				
15 -			- 427	11		3.5					
	- soft CLAY (lean) with SAND, trace gravel, st medium plasticity, dark yellow brown	iff to hard,	-	13		2.0	CL				
20 -				14	60/60						

	KELRON ENVIRONMENTAL INCORPORATED		L	.OG	OF	BOF	RING N	/W-25	5 3 (Page 2 of 2)
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. n: Twp 04S, Rng 07W, 15 SW, SW, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company		'OD / 4 w-Sten	-	(CME-55	Top of	Surface Elev	: Matt Cooper : Brendon Wilder (PSC) vation: 442.70 vation 445.84 : 2384430, 553298
Depth in Feet	DESCRIPTION		Surf. Elev. 442.70	Samples	Recovery inches	Qp TSF	USCS	Well Elev	l: MW-253 7.: 445.84
20 -	- grain size analysis @ 19 - 19.5 ft: 0.7% gravel, 26.9% sand, 38.1% s	ilt, 34.3% clay	- 422	14	60/60				
- 25 -	- small fine sand seams from 25 to 2		- 417	15	60/60		CL		Grout Bentonite Slurry Riser (Sch 40 PVC)
	CLAY (fat), shaley, platy/laminated, soft light yellow brown (10YR 6/4) - stiff to very stiff, light olive brown (2 - grain size analysis @ 29 - 30 ft: 6.7% sand, 21.6% silt, 71.7% clay			16 17 18	60/60				
-	- Drove split-spoon 2-inches into bec	Irock: 34 5 to	- 412	19 20		3.5 3.0	СН		Filter Pack
35 - -	34.7 feet bls LIMESTONE with SHALE Auger refusal at 35.0 feet END BOREHOLE AT 35.0 FEET BLS		- 407	21-	2/2		S/SH		Bottom Cap
40 -									

Illinois Environmental Protection Agency

Well Completion Report

Incident No.: None		Well No.: <u>MW-153</u>							
Site Name: Dynegy-Bal		Date Drilled Start: 09/21/10							
Drilling Contractor: <u>Te</u>	rra Drill	Date Completed: 09/21/10							
Driller: <u>Matt Cooper</u>		Geologist: Brendon Wilder							
Drilling Method: <u>Hollov</u>	v-Stem Auge	Drilling Fluids (Type): <u>None</u>							
Annular Space Details					Elevations01 ft. Top of Protective Cas				
Type of Surface Seal: <u>Co</u>	ncrete	15			445.67 Top of Riser Pipe				
Type of Annular Sealant:	Bentonite C	hips			442.77 Ground Surface				
Type of Bentonite Seal (G	iranular, Pe	llet):			441.77 Top of Annular sealar				
Bentonite Chips (hydrated)					Casing Stickup				
Type of Sand Pack: Clear	1 Silica Sand	1							
Well Construction Materia	ale								
wen construction materia			-	r I I I I					
	<u> </u>	/pe	be						
	Typ.	Ţ.	Ĺ.						
	ify .	C if	cify t		436.07 Top of Seal				
	Stainless Steel Specify Type	PVC Specify Type	Other Specify Type		2.00 Total Seal Interval				
Riser coupling joint			0 8		 Construction of the second s Second second seco				
Riser pipe above w.t.				M M	434.07 Top of Sand				
Riser Pipe below w.t.		Sch. 40							
Screen									
201001	\$	Sch 40			432.42 Ton of Samon				
	£	Sch. 40			432.42 Top of Screen				
Coupling joint screen to riser Protective casing	£	Sch. 40			4 <u>32.42</u> Top of Screen				
Coupling joint screen to riser Protective casing Measurements	to .01 ft (w		licable)		4 <u>32.42</u> Top of Screen				
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length					4 <u>32.42</u> Top of Screen				
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length		here app			4 <u>32.42</u> Top of Screen <u>9.64</u> Total Screen Interval				
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size		here app 13.25							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length		here app 13.25 9.25							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water		here app 13.25 9.25							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water		here app 13.25 9.25 0.01							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness		here app 13.25 9.25 0.01 16.38							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water		here app 13.25 9.25 0.01 16.38							
Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness		here app 13.25 9.25 0.01 16.38 429.29							

Illinois Environmental Protection Agency Well Completion Report Incident No.: None Well No .: MW-253 Site Name: Dynegy-Baldwin Energy Complex Date Drilled Start: 09/20/10 Drilling Contractor: Terra Drill Date Completed: __09/20/10 Driller: Matt Cooper Geologist: Brendon Wilder Drilling Method: Hollow-Stem Aug.; Mud-Rotary Drilling Fluids (Type): Water w/ Polymer Annular Space Details Elevations - .01 ft. _ Top of Protective Casing Type of Surface Seal: Concrete 445.84 Top of Riser Pipe Type of Annular Sealant: Cement-Bentonite Grout 442.70 Ground Surface Type of Bentonite Seal (Granular, Pellet): 441.70 Top of Annular sealant Bentonite Chips (hydrated) _ Casing Stickup Type of Sand Pack: Clean Silica Sand Well Construction Materials Specify Type Type Stainless Steel Specify Type Other Specify 417.00 Top of Seal PVC 2.00 Total Seal Interval Riser coupling joint 415.00 Top of Sand Riser pipe above w.t. Sch. 40 Riser Pipe below w.t. Sch. 40 Screen Sch. 40 412.84 Top of Screen Coupling joint screen to riser Protective casing Measurements to .01 ft (where applicable) **Riser Pipe Length** 33.01 Screen Length 4.63 4.63 Total Screen Interval Screen Slot Size 0.01 Protective casing length Depth to water 12.71 Elevation of water 433.13 Free Product thickness Gallons removed (develop) 7.89 Gallons removed (purge) Other 408.21 Bottom of Screen 407.70 Bottom of Borehole

Completed by: PSC Industrial Outsourcing, LP

	KELRON ENVIRONMENTAL		L	.OG	OF	BOR	ING N	1W-35	2
	INCORPORATED								(Page 1 of 3)
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. on: Twp 04S, Rng 07W, 16 SE, NE, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: Hollov	'OD / 4 w-Sten		(CME-55	Top of	urface Elev	: Matt Cooper : Brendon Wilder (PSC) ration: 422.36 vation: 425.04 : 2382789, 553901
Depth in Feet 0 -	DESCRIPTION SILTY CLAY, very stiff to hard, yellow b 5/6), dry	rown (10YR	Surf. Elev. 422.36	Samples	Ae/48	4.5+	USCS	Well: Elev.	: MW-352 : 425.04 Cover Concrete
- 5 - - -	CLAY, trace sand and fine gravel, very plasticity, few black organic material	stiff, high	- 417	2 3 4 5	60/60	3.5 4.0 2.75 3.0			
- 10 - - -	- medium hard - soft		- 412	6 7 8	60/60	2.75 2.0 1.0	CL		· · · · · · · ·
- 15 - -	- medium hard	a thial)	- 407	9 10 11	60/60	1.25 1.5 2.5	SP C:		Bentonite Slurry Riser (Sch 40 PVC)
- 20 - - -	SAND, poorly graded, loose, wet (4-incl SANDY CLAY, trace fine gravel, yellow brown (2.5Y 5/3)		- 402	12 13 14 15 16	60/60	2.75 3.5 4.5+ 2.5 2.5	CL		
- 25 -				17 18	48/60	2.75 2.5			•

	KELRON ENVIRONMENTAL INCORPORATED		L	OG	OF	BC	RIN	G M\	N-3		age 2 of 3)
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. on: Twp 04S, Rng 07W, 16 SE, NE, NE	Hole Diameter : 8 1/2"OD / 4 1/4" ID: 3 7/8" rock G Drilling Method : Hollow-Stem/Rotary (CME-550) La Sampling Method : MacroCore (60")/NX Core					Driller : Matt Cooper Geologist : Brendon Wilder (PSC) and Surface Elevation: 422.36 Fop of Casing Elevation 425.04 (,Y Coordinates : 2382789, 553901				
Depth in Feet	DESCRIPTION		Surf. Elev. 422.36	Samples	Recovery inches	Qp TSF	NSCS	GRAPHIC		ell: MW ev.: 425	
25 -	- grain size analysis @ 26.5 - 27.5 ft 33.7% sand, 27.1% silt, 39.2% cla SAND with few gravel, yellow brown	y/	- 397	18	48/60	2.5	CL				
- 30 - -	CLAY, some sand and fine gravel, hard high plasticity, dark yellow brown (10YR CLAY, lean to fat	to very nard, 4/6)	- 392	19 20	60/60	3.0 3.0	CL				
-	- grain size analysis @ 32 - 33 ft: 13.2% sand, 43.9% silt, 42.8% cla	у		21 22		3.5 3.0					
35 -	 medium hard, high plasticity, gray b olive brown (2.5Y 5/2-5/3) trace silt, dark yellow brown (10YR) 		- 387	23 24 25 26	48/60	1.5 1.5 1.75 1.5	CL/CH	+			Grout Bentonite Slurry
40 -			- 382	27 28	54/60	1.75 2.0					Riser (Sch 40 PVC)
- - 45 - - -			- 377	29 30 31 32	57/60	2.5 2.5 2.0 1.75					
	CLAY, medium hard, low plasticity, olive 5/4)	e brown (2.5Y	-	33 34 35 36	3/3	1.75 2.5 1.75	CL				
50 -]		0/0				* • •		

	KELRON ENVIRONMENTAL INCORPORATED		L	.OG	OF	BOF	RING	g mv	V-35	2 (Page 3 of 3)
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. on: Twp 04S, Rng 07W, 16 SE, NE, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: Hollov	'OD / 4 w-Sterr	4 1/4" ID n/Rotary (60'')/NX	(CME-5	rock G 50) L T		sing Ele	: Matt Cooper : Brendon Wilder (PSC) ration: 422.36 vation 425.04 : 2382789, 553901
Depth in Feet	DESCRIPTION		Surf. Elev. 422.36	Samples	Recovery inches	Qp TSF	NSCS	GRAPHIC		: MW-352 :: 425.04
50 -	- Auger refusal at 53.7 feet bgs		- 372				CL			
- 55 -	LIMESTONE, weathered, thinly laminate hard to hard, gray	ed, medium	- 367	37 38	5/5 8/27		LS			Grout Bentonite Slurry
	SHALE, clayey, gray LIMESTONE, occasional shale partings		-	39	19/60		SH			
-	- laminated, fossiliferous, medium gr	ay	- 362				LS			Riser (Sch 40 PVC)
65 -	SHALE, soft, dark gray		- 357	40	54/60		SH			Bentonite Chips
- - 70 - -	LIMESTONE, medium hard to hard, ligh		-	41	59/60					Filter Pack
70 -	Borehole diameter from 53.7 to 73.8 fee RQD for 53.8 - 73.8' = 57% (Fair) Recovery = 173/240"	t bgs = 3 7/8"	- 352	42	33/34		LS			Screen (pre-pack)
- 75 -	END BOREHOLE AT 73.8 FEET BLS									

Illinois Environmental Protection Agency Well Completion Report Incident No.: None Well No.: MW-352 Site Name: Dynegy-Baldwin Energy Complex Date Drilled Start: 09/15/10 Drilling Contractor: Terra Drill Date Completed: __09/17/10 Driller: Matt Cooper Geologist: Brendon Wilder Drilling Method: Hollow-Stem Aug.; Mud-Rotary Drilling Fluids (Type): Water w/ Polymer Annular Space Details Elevations - .01 ft. Top of Protective Casing Type of Surface Seal: Concrete 425.04 Top of Riser Pipe Type of Annular Sealant: Cement-Bentonite Grout 422.36 Ground Surface Type of Bentonite Seal (Granular, Pellet): _ 421.36 Top of Annular sealant Bentonite Chips (hydrated) Casing Stickup Type of Sand Pack: Clean Silica Sand Well Construction Materials Type Specify Type Stainless Steel Specify Type Other Specify 361.06 Top of Seal PVC 4.00 Total Seal Interval Riser coupling joint 357.06 Top of Sand Riser pipe above w.t. Sch. 40 Riser Pipe below w.t. Sch. 40 Screen Sch. 40 354.46 Top of Screen Coupling joint screen to riser Protective casing Measurements to .01 ft (where applicable) **Riser Pipe Length** 70.59 Screen Length 4.63 4.63 Total Screen Interval Screen Slot Size 0.01 Protective casing length Depth to water 23.85 Elevation of water 401.19 Free Product thickness Gallons removed (develop) 13.70 Gallons removed (purge) Other 349.83 Bottom of Screen 348.56 Bottom of Borehole Completed by: PSC Industrial Outsourcing, LP

ATTACHMENT 4

Location of CCR Porewater Piezometers TPZ-163, TPZ-167, and TPZ-168



- HONITORING WELL AND PIEZOMETER LOCATIONS
- ABANDONED MONITORING WELL AND PIEZOMETER LOCATIONS
- PART 845 REGULATED UNIT (SUBJECT UNIT)
- FLY ASH POND SYSTEM (CLOSED)

SITE FEATURE LIMITS OF FINAL COVER PROPERTY BOUNDARY

MONITORING WELL LOCATION MAP

FIGURE 2-1

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS